### Rockfall Hazard Classification and Mitigation Phase 1

(Cooperative Transportation Research Program: University of Idaho and the Idaho Transportation Department)

**Summary Report** 

Prepared for

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#### INTRODUCTION

The Federal Highway Administration (FHWA) began a concerted effort in the 1980's to address rockfall hazards along highways as part of its overall mission to improve highway safety. The Oregon Department of Transportation (ODOT) took the lead in developing and testing various data collection procedures for a standardized Rockfall Hazard Rating System (RHRS). A fairly comprehensive study of rockfall sites along Oregon highways in 1989-91 included approximately 3,000 rock cuts and was used as the final stage of development and testing of the RHRS. Results of this extensive work were summarized and adapted into a training manual for the National Highway Institute Course No. 130220 (FHWA Publication No. SA-93-057, November 1993: Rockfall Hazard Rating System).

Several Western states (including Arizona, Colorado, and Washington) have since joined Oregon in the implementation of highway rockfall hazard rating and mitigation programs in line with these FHWA guidelines. The goals of such programs are: 1) to improve highway conditions for enhanced public safety and rockfall maintenance (cleanup) planning/budgeting, and 2) to identify and prioritize rockfall hazard sites, so that highway funds can be allocated efficiently for construction projects or counter-measures to mitigate the hazards. A systematic rockfall hazard assessment has not been completed for Idaho highways, though significant efforts to inventory and describe rockfall sites have been initiated by individual Idaho Transporation Department (ITD) personnel in the past five years (especially in ITD Districts 3 and 6).

This current research program is intended to assist ITD with a systematic evaluation of rockfall hazards along Idaho highways and with the development of a computer database useful for cataloging, sorting, and prioritizing rockfall-prone sites. The approach is based on earlier FHWA work that recommended a two-step process for rockfall hazard ratings: 1) a preliminary rating to categorize slope segments as having a high, moderate, or low potential of rockfall on the roadway; and 2) a detailed hazard rating based on the RHRS developed by the Oregon DOT for FHWA.

The primary specific tasks addressed during Phase 1 (1999-2000) of this Idaho rockfall research project were:

- 1. A rockfall maintenance survey form was designed and distributed to road maintenance personnel in each ITD district, so that local ITD personnel could identify known rockfall areas and help prioritize them for further study and treatment.
- 2. Rockfall hazard rating systems based on available FHWA procedures and those from several western states were reviewed and then adapted for use in Idaho. The key modifications involved traffic (load) volume and maintenance/remediation efforts.

3. Trial field evaluations using the Idaho rockfall hazard rating system originally were planned only for ITD Districts 2 and 3, but several field sites actually were analyzed in each of the six Districts.

Project coordinators and representatives from ITD for this project were:

Mr. Robert Smith Research Supervisor P.O. Box 7129 Boise, Idaho 83707

Mr. Keith Nottingham Engineering Geologist, District 3 P.O. Box 8028 Boise, Idaho 83707

Mr. Bryon Breen Roadside Maintenance Office P.O. Box 7129 Boise, Idaho 83707

#### ROCKFALL INVENTORY SURVEYS

As a means to identify rockfall problem areas along Idaho's highway systems, a comprehensive inventory procedure needed to be implemented. Because highway maintenance crews are very familiar with rockfall cleanup history and frequency, a rockfall survey form (field sheet) was developed for crew members to fill out for highway segments located within their operating work areas. This survey form is based on a scheme slightly different from that used in the preliminary rockfall hazard rating system used by the Oregon DOT.

The Oregon preliminary rating system (Publication No. FHWA SA-93-097, 1993) was based on two criteria: 1) estimated potential for rockfall on roadway, and 2) historical rockfall activity. The potential for rockfall is the primary key for classifying the rock slope, with the historical evidence used as a supplement when further clarification is needed. The classes for rockfall hazard are given by "A" (high), "B" (moderate), "C" (low). None of the C-rated slopes in the Oregon study were investigated further, because, as the FHWA Publication states, "... the risk of a hazardous situation occurring [for a C slope] is nonexistent-to-low" and it was deemed "... not worthwhile to clutter the database with information on slopes of this nature." Only the A-rated (a total of 501 slopes) and B-rated (a total of 839 slopes) rock slopes in Oregon were analyzed further using the more detailed Rockfall Hazard Rating System (RHRS).

Our approach to the preliminary rockfall rating scheme in Idaho was to include only those rock slopes that 1) had a history of delivering rockfall debris to the roadway, or 2) those slopes that had a significant potential to deliver debris to the roadway even if no rockfall cleanup had been conducted there before. These rock slopes were assigned a preliminary rockfall hazard classification on the survey forms using the following severity scale:

- 1 -- Rockfall debris occasionally sloughs onto the roadway, and the deposited material usually is less than a few inches (10 cm) in mean diameter.
- 2 -- Rocks with a mean diameter of up to 6 inches (15 cm) land on the roadway several times a year, causing hazardous driving conditions during some of these events.
   There is a potential for even larger rocks up to 18 inches (45 cm) to hit the roadway during severe storm events.
- 3 -- Rocks are deposited on the roadway frequently or in such a manner that would produce hazardous driving conditions (such as rockfall on a blind curve). Such sites likely will need cleanup attention by maintenance crews during or immediately after storm activity. Other recognizable site features include: potential catastrophic failure of the rock slope, a likelihood of large rocks (greater than 18 inches) reaching the roadway, or noteworthy geologic features that potentially could generate sizable volumes of rockfall debris.

ITD materials personnel in Districts 3 and 6 already had completed some preliminary rockfall "mapping" in recent years; this available information was incorporated into the survey database. New rockfall inventories were conducted in the remaining Districts during 1999 and 2000 either by ITD maintenance personnel or by University researchers.

The data sheet used to record the rockfall sites is presented in Appendix A. Copies of the individual data sheets for each District also are given in Appendix A. Results of the rockfall survey are summarized in Table 1.

Table 1. Summary of rockfall survey data and preliminary assessment of rockfall severity.

	Total Number	Rockfall Severity Rating (Number of Sites)				
ITD District	of Rockfall Sites	1	2	3		
1	167	116	17	34		
2	310	104	136	70		
3	125	54	46	25		
4	216	120	61	35		
5	83	52	25	6		
6	86	18	53	15		

In addition to the above information, the "worst" rockfall sites were identified based on comments from ITD maintenance personnel or based on the high-hazard potential of areas that may not have a history of significant rockfall cleanup. These sites represent those areas most worthy of receiving future rockfall mitigation efforts, as indicated by the preliminary rockfall hazard assessments:

District	1		District	2		District	<u>3</u>
SH 3	mp 55.0		US 12	mp 33.45		US 95	mp 144.6
	mp 73.7			mp 56.45			mp 173.6
SH 5	mp 10.0			mp 76.0			mp 175.1
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:	mp 96.0			mp 133.8		SH 55	mp 67.7
SH 200	mp 41.5			mp 159.6			mp 76.5
	mp 56.1			mp 168.5			mp 80.7
				mp 172.4			mp 91.9
			US 95	mp 198.0			mp 93.5
				mp 231.2			mp 94.2
				mp 286.2			mp 150.2
			SH 7	mp 51.0			mp 150.6
			SH 11	mp 4.2			mp 151.9
			SH 13	mp 14.5			
				mp 19.4			
			SH 14	mp 7.6			
				mp 10.1			
				mp 12.9			
				mp 16.6			
				mp 33.0			
				mp 42.0			
District	4		District	<u>5</u>		District	<u>6</u>
SH 75	mp 155.7		US 89	mp 35.8		US 26	mp 374.5
	mp 199.2			mp 37.1			mp 389.0
	mp 202.1		SH 34	mp 26.0		US 93	mp 264.0
	mp 203.0		SH 36	mp 114.6			mp 273.5
	mp 205.1						mp 281.6
	mp 208.3						mp 283.3
	mp 213.1						mp 319.5
	mp 220.8						mp 324.5
						SH 47	mp 11.6
						SH 75	mp 224.0

#### ROCKFALL CLASSIFICATION AND HAZARD RATINGS

The Rockfall Hazard Rating System (RHRS) developed by the Oregon DOT for FHWA (FHWA Publication No. SA-93-057, November 1993) included ten rating categories, four of which were based on slope and road geometry, three based on geologic factors, one based on climate, one based on average vehicle risk (a function of traffic volume, travel length of rockslope exposure, and posted speed limit), and one based on rockfall history. Each category was divided into four classifications which received numerical scores based on an exponential weighting system: 3 points for low impact on rockfall hazard, 9 points for moderate impact on rockfall hazard, 27 points for moderately high impact on rockfall hazard, and 81 points for high impact on rockfall hazard. After measuring and scoring a given rockfall site, the ten category scores then were summed to give a total rockfall hazard score, with a higher score indicating greater rockfall hazard.

Rockfall rating categories used in the RHRS are listed below:

- 1. Slope height (vertical height of slope measured in feet);
- 2. Ditch effectiveness (rated according to catchment effectiveness);
- 3. Average vehicle risk;
- 4. Percent of decision site distance (function of posted speed limit), as calculated by the ratio of actual site distance to the decision site distance, expressed as a percent;
- 5. Roadway width including paved shoulders;
- 6. Geologic structural condition (case 1 for hard rock, case 2 for differential erosion);
- 7. Geologic shear strength (rock friction, case 1) or erosion rates (case 2);
- 8. Size of rock blocks or volume of rockfall event;
- 9. Climate and presence of water on the slope; and
- 10. Rockfall history.

This basic format has been retained for the Idaho rockfall hazard rating system, but we have followed more closely the modified scoring system used by the Arizona DOT, which simplified the original RHRS to require fewer numerical calculations (such as those used for the RHRS average vehicle risk and decision site distance). Also, the proposed Idaho rockfall rating scheme has been separated into two major subdivisions, one that describes the physical hazards at each rockfall site and one that describes the potential risk (associated with personal injuries, loss of life, or financial losses/costs). The Idaho rockfall rating categories are described below:

Sources of physical hazard (potential for damaging rocks to land on the roadway)

- 1. Slope continuity (severity of rockfall launching features on the slope);
- 2. Size of rock blocks:
- 3. Dimensions of catch-ditch;
- 4. Geologic factors (hard rock outcrops, case 1; differential erosion features, case 2);
- 5. Climate and precipitation factors; and
- 6. Rockfall history (frequency of rockfall on the roadway).

Sources of risk (personal injuries and loss; maintenance costs)

- 1. Traffic volume based on Average Daily Traffic (ADT) counts;
- 2. Sight distance (distance needed for a motorist to see and avoid a 6-in. object);
- 3. Roadway width including paved shoulders (avoidance room for motorists); and
- 4. Maintenance and cleanup efforts/costs.

The rockfall hazard evaluation form currently being tested for Idaho roadways is presented in Appendix B. The slope height category in the original RHRS has been replaced with the slope configuration criteria, because height alone does not provide a unique measure of a rockslope's potential to deposit rock debris on a roadway. For example, a 50-ft high vertical rock cut with a reasonable catch-ditch (say, 15 ft) presents less of a hazard than a 30-ft high 1:1 rock cut with one or more launching features and the same catch-ditch width. Another difficulty in measuring slope height in the field is the ambiguity inherent in trying to distinguish rockfall originating from the artificial cutslope and that originating farther uphill on a steep natural slope.

During the summer of 2000, University personnel used these rockfall evaluation forms to rate 60 rockfall sites in Districts 1-5. Sites in District 6 previously had been rated by ITD personnel using a different evaluation procedure; adjusting and adapting these earlier rockfall hazard scores is currently under evaluation. It was our initial goal in each District to apply this detailed rating scheme on six sites that scored a severity "3" on the preliminary rockfall survey, on three sites that scored "2", and on three sites that scored "1". This plan was altered for District 5 due to its lack of readily accessible severity "3" sites. A statistical summary of the rockfall hazard ratings is given in Table 2.

These results indicate the general consistency between the rockfall survey scores and the rockfall hazard rating scores. That is, generally the sites with rockfall severity "1" had the lowest hazard rating scores and those with severity "3" had the highest hazard rating scores. The exception to this relationship is for the sites in District 1, where the severity "1" rock slopes scored unusually high on the overall rockfall hazard rating system.

For all 60 sites combined, the <u>physical hazard</u> ratings ranged from 41 to 387 (only mean values are shown in Table 2), with a score greater than about 200 indicating fairly high hazard. The <u>risk</u> ratings ranged from 12 to 138 (only mean values are shown in Table 2), with a score greater than about 100 indicating fairly high risk. Thus, even with this limited sample of rockfall sites around the state, we can begin to see that an overall rockfall hazard rating of 300 or greater (i.e., 200 + 100) likely is indicating that such sites are a high priority for future mitigation efforts.

These initial results also suggest that a simpler, streamlined version of the rockfall hazard rating system may be applied to provide similar outcomes in terms of priority rankings. For example, two key terms in the physical hazard rating categories are catch-ditch dimensions and rockfall history. Scores from these two categories could be added to the risk ratings to obtain a modified total score (excluding slope continuity, size of blocks, geologic factors, and

climate). However, some confusion may arise regarding a rock slope that poses a significant potential hazard by its geometry above the roadway, but actually has very little rockfall history. To handle this situation, the category for rockfall history could be changed to include "rockfall history" or "potential for a major one-time rockfall event."

Another possible approach is to use a two-fold criteria for assessing rockfall mitigation priorities. An example would be where the highest-priority sites could be identified by "a risk score greater than 125, or a risk score greater than 100 and a hazard score greater than 250." Such modifications to this initial rockfall hazard rating system for Idaho need to be investigated further.

Table 2. Summary of rockfall hazard ratings for trial sites along Idaho roadways.

ITD	Initial Rockfall	No.	Ro	ckfall Hazar	d Rating	Scor	es	
District	Severity Rating	Sites	Risk Mean	Haz.Mean	Total:	Min.	Max.	Mean
1	1	4	81	181		96	351	262
	2	3	93	82		97	235	175
	3	6	85	188		154	387	273
2	1	3	60	110		93	211	170
	2	3	61	126		109	328	<b>187</b>
	3	5	56	166		159	344	222
3	1	3	51	112		137	207	163
	2	3	65	142		105	285	207
	3	6	64	262		177	407	326
4	1	3	49	192		105	387	241
	2	3	67	217		265	315	284
	3	6	65	311		247	501	<b>376</b>
5	1	6	35	69		63	171	104
	2	4	49	96		99	201	145
	3	2	93	222		285	345	315
Totals	1	19	55	133				188
	2	16	67	133				200
	2 3	25	73	230				302

#### DATABASE DEVELOPMENT

Though not a part of the original work tasks on this project, development of a computerized database of rockfall hazard information has been initiated using Microsoft ACCESS-2000. Two data tables have been constructed to date: one consisting of the rockfall survey data with the severity scores (1, 2, 3) and the other consisting of the 60 sites where the more detailed rockfall hazard ratings were obtained. Digital photograph images also were obtained at all 60 sites, with the intent of including such image files as attachments or tags in the Idaho rockfall database. Due to the massive data storage requirements for these images, it is likely that they will be converted to "jpeg" or "pdf" files and placed on a website that can be accessed from the core database.

There are also "size of record" problems associated with large data tables within ACCESS. Thus, we are working to develop several internal switchboards through which users can navigate through the database and sort out the information they need, such as: identifying those rockfall sites in a District that have a risk rating greater than 125 and a rockfall history score (or potential one-time event score) of 27 or greater.

Much additional work is needed to develop a working rockfall database for ITD use. This activity is included as a task item in the proposal for Phase 2 work on this project.

#### CONCLUSIONS AND RECOMMENDATIONS

Rockfall maintenance surveys have been completed for roadways in all six ITD Districts. Based on rockfall history and cleanup activities, the most severe rockfall problems occur in Districts 2 and 3, followed by Districts 1 and 6. Follow-up rockfall hazard ratings were conducted on about 12 sites in Districts 1-5 using the Idaho rockfall hazard rating system, which was adapted from the method used by the Arizona DOT. These preliminary results suggest that the Idaho system may be simplified and still retain an adequate quantitative sensitivity to rank and prioritize rockfall hazards.

The three proposed work tasks in Phase 1 were completed. In addition, we began development on an ACCESS database that will contain Idaho rockfall hazard information and digital images of selected sites around the state. More field work is needed to gather additional rockfall hazard data and more office work is needed to expand the data and operational flexibility of the database.

Proposed work tasks for Phase 2 of this project (2000-2001) are described below:

Task 4. Based on information provided from the Phase 1 rockfall studies completed statewide, roughly 6-10 sites will be identified for further study in each District. These sites will be evaluated using the Idaho rockfall rating system and one or more of its modifications as suggested from the Phase 1 work.

- Task 5. Collect and organize cost data and other case study information on rockfall mitigation projects recently completed in other Western states. This will supplement and update the information presented by FHWA in the rockfall course notes printed in 1993-94. This compilation will provide ITD with useful information for rockfall project design and costestimation.
- Task 6. Organize and input the rockfall inventory and hazard rating information, as well as the cost data, into a computer data base that can be readily accessed by ITD personnel.

A final report will summarize the rockfall project and make recommendations for hazard mitigation along Idaho highways. Not all rockfall sites in the state will be rated during this project, and some follow-up work by ITD or NIATT personnel will be needed to complete the hazard rating statewide.

## Appendix A

Field Sheets for Rockfall Inventory Surveys

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DISTRICT		ORG UNIT:	DATE: ORG LOCATION:					
E-MAIL:			TELEPHONE:					
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS				
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- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
- 2. Rock debris occurs on the roadway several times a year with the larger rocks (> 6 inches) causing hazardous conditions during some of these events.
- 3. Rock debris occurs on the roadway frequently or in such a manner that would create a hazardous condition, such as rockfall on a curve. Such locations often require immediate attention during or after storm activity.

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- 2. Rock debris occurs on the roadway several times a year with the larger rocks (> 6 inches) causing hazardous conditions during some of these events.
- Rock debris occurs on the roadway frequently or in such a manner that would create a hazardous condition, such as rockfall on a curve. Such locations often require immediate attention during or after storm activity.

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- 3. Rock debris occurs on the roudway frequently or in such a manner that would create a hazardous condition. such as rockfall on a curve. Such locations often require immediate attention during or after storm activity.

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	12	DISTRICT:_ E-MAIL:	<i>F</i> ,	.0 0,	TELEPHONE:	208.77	12 - 1211	BILL CA	Puul	
	State of the state	T.		-						
5491	7	ROUTE	BEGIN ML.P.	END M. P.	SEVERITY (1-3)					
	78	Hwy- 49)	95.930	96033	3	IRT OF	E Bedroe	K SOME	may	& Kul
	79	1.07	95.741	95.750	3	1		Direch	Occ.	rock
	 g∂		95504	95671	3		3' Ditel		/-	
	9/		94,142	97.444	3		Varible	Dreb	$-\!$	
	82		93.009	93.495	3		3'			
	-		92.346	97,00	,		3'			
	93			92.295	1	F	Varible	Ditch		
	84		92.048	84730			No D17	•	1	
	85		84.682	AND DESCRIPTION OF THE PERSON		1	1,			
	96		84445	84.519	1	11	3'			
	87		82,476	82 556		RT.	3'			
	38		81.857	82.046	/		3.			
	99		A1.939	21985	/	LTI			7	
	90		81.182	81,2110	1	RT.	31			
	91		73,180	73. 251	/	12T	3'	<u> </u>	. //	
	92		73 232	73.592	/	Rr	3'	Cochoin		
	93		72.105	72,193	1	ÈT.	?	Be	Irack	
	94		71,702	71.762	,	RT	<u> </u>	• /	-	
	95		70.258	70.330	3		LF 5' DI	reh	+	
	96		69.049	69.15	1	157	Marible			
			66.718	66972	2	13	VArible	Direk		
	97		66.460	66,648	Z	1	5'			
	928 99		66.355	66.385	Z	11	S		1	
			(bla 0)	(ab. 126)	1	1	3		(	
>	100		(Colon O)	ENC						
				1 _//-						
		8			1					

NOTES: ANY TYPE WEATHER CONLITIONS CAUSES SERIOD; FORE FALL
ON This STrench of Road, MP 96,013 TO 92.048

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
- 2. Rock debris occurs on the roadway several times a year with the larger rocks (> 6 inches) causing hazardous conditions during some of these events.
- 3. Rock debris occurs on the roudway frequently or in such a manner that would create a hazardous condition, such as rockfall on a curve. Such locations often require immediate attention during or after storm activity.

E-MAIL		-dh: ) ( 2	END M. P.	SEVERITY (1-3	) ADDITI	ONAL COMMENTS	
ROUTE			70.837	1		F & NO DITE	Bedi
>" PHWY-	and the same of the same of	70.760	71.36?	1	1	Eward Rin U	٦ حرا
102	_	71.218	71.690	3	)	3-15' Varible To	itch
714		73.581	73.911	3	LT.	3 1-18/Arible	
105		73.958	74.069	1		Z' Direh	
106		74.111	74 218	1		L. NITA	
107	++	78,807	78.852	2		3' DITCH	
108	++	79.163	79.189	ζ	11	<b>b</b> '	
109	++	79 321	79. 385	2	11	3	
110	++	79.485	79.508	2	RT	2'	
"		80.011	80.115	L	RT	2'	
112	-	80.249	80.292	2	15-	5'	
113		20.459	80.680	2	ित	6'	
119		80.767	80.940	2	12	6'	
185		81.141	81.194	2	10	3'	
116		83.704	33.805	2	127	8'	110
117		92.517	92.727	2	LT.		W/Collo
118		92.784	94.0	2	+(-	3 (Be	brock
119		94551	94.629	2	Rr		ivium _
320		101.168	101.5		1 3		rock
一团 ]		104.312	104.369	1	+ /	3' /	
122		105.50	165,788	1	+	3 /-	
123		109.0	109.237		+)	91	
139		111,180	111.267	<del>                                     </del>	LT.	6' 1	

1	MO ( 82:			
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ROUTE	BEGIN M. P.		SEAFIGIA (1-2)	ADDITIONAL COMMENTS
HWY- 3	68.962	69.037	<u> </u>	KT. EFE ( & Directi Call
	F/2 160	56.172		IT ask with Redra
	55 975	55.994		/ Varible
	55.718	75413		3.7.24
)	54.797	35.13e	3	I strible
		ENZ		
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	<u> </u>			
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OTES:				
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11-1-99 EVALUATED BY: Ken 90 TO MONTANE LINE ORG LOCATION: INTERITATE DISTRICT: 67 BILL CAPINUL TELEPHONE: 208-772-1211 E-MAIL: SEVERITY (1-3) ADDITIONAL COMMENTS END M. P. BEGIN M. P. 9'DIRL Balrack W/The strand ROUTE RT. OF E 18.976 181 16.953 18-36' Ditch. Helrock į 19.69 18.759 132 NO DITE A RODOCE: 5700 6:00 20.853 £33 ZO. B4E 10' DIRA 21.365 21.360 139 21.530 21.525 135 91 21,555 21,551 136 24.654 24.798 10, 137 25.297 PEROCK 25.232 10' Varible Ditch 138 Rr 25.888 25.861 139 LT. 26.058 25.934 140 12' Bedrock RT. 26.230 24.090 141 12' DITch LT. 29,926 29.840 Varible Ditch 142 RT 30.408 30.375 143 5 30 977 30,951 149 10' Direli 31.846 31,795 12' Direk Sedrock 145 63.234 63.200 146 12' 67,549 63.351 Varible Ditch 147 3 63.802 63.718 20'DITCH GUARD RAIL W/2' Free e sepret 148 3 67.020 66.962 149 12' DIrch 67.161 3 67.086 150 3' 67.251 1 67.188 151 COLLUVIUM 15' 71.180 71.098 152 12' 71.374 71.281 153 15'

NOTES:				

15'

71.763

72,168

71669

72.0

#### SEVERITY:

159

155

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
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		END M. P.	SEVERITY (1-3)	ADDITIONAL C	OMMENTS	
	BEGIN M. P.	72.793	1	The state of the s	15' Direch	i en
I-90	72.708			110.00	18' (	1.5(
{	72.911	72.968	15	<del>i                                    </del>	12'	<del></del>
}	73.119	73.190		<del>                                     </del>		
	1					
		1				
		<u> </u>			-	
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						7
OTES:				•		
					<b>4</b> , 1	
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HWY-Y 1.270 1.38/ 1 LT. OF £ 2' DITCH    3.706 3.739	ROUTE	BEGIN M. P.	ENO Yr. 5.		ADDITIONAL CO	MINICIVIS
3.775 3.789 3' 4.280 4.31 NO DITCH  4.643 4.662 3' 4.67c 4.721 3' 4.878 4.948 3' 5.795 5.864 3 RT. CF & NO DITCH	HWY-4	1. 270	1.381	/	L1. 0 F &	Z DITER 1
4.280 4.31 NO DITER  4.643 4.662 3'  4.676 4.721 3'  4.878 4.948 3'  5.795 5.864 3 RT. CF & NO DITER	1			++	+ /	
4.643 4.662 3' 4.676 4.721 3' 4.878 4.948 3' 5.795 5.864 3 RT. CF & NO DITCH		The second secon	Carlo State		+-(	
4.878 4.948 3' 4.878 4.948 3' 5.795 5.864 3 RT. OF & NO DITCH		4. 280		1	1-1-	NO UTON
4.878 4.948 3' 5.795 5.864 3 RT. OF & NO DITCH			of the last section is not a second or the last section is not a section is not a second or the last section is not a second or the last section is not a second or the last section is not a section is not a second or the last section is not a second or the last section is not a section is not a second or the last section is not a second or the last section is not a se			J
5.795 5.864 3 RT. OF & NO DITCH			The state of the s	11	+	
J. 113 Jan Arad		4.878		1		
6.671 6.590 1 RF. NO BITCH		5.795		7		Na Direct
		6.671	6,590	11	\RF	NO DITEM
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		- 1-90 s				
	NOTES:					
NOTES:						

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E-MAIL:	BEGIN M. P.	ENO M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
Hwy.95		425.253	3	RT OF & 9' NITCH BELLICA
> 5	424 759	1424.90	1,	RT OF & 9' NITCH BELLION  CONCrete GUARD Zail Zo VANIL
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VOTES:				

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
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EVALUATED BY: BLAKE THOMPSON ORGUNIT. 270 OR		RIBUF	- THOMPSON	<u>4</u>	DODE IND
ROUTE BEGIN M. P. SEVERITY (1.3) ADDITIONAL COMMENTS  US 12 24.0 < 24.7/ 3  26.0 26.0	EVALUATE DISTRICT	2 _0	IG UNIT: 270	ORG LOCATION:	18-476-4433
ROUTE BEGIN M. P. SEVERITY (1.3) ADDITIONAL COMMENTS  US 12 24.0 < 24.7/ 3  26.0 26.0 / 1  28.11 28.13   Barrier after Road  30.22 30.27 3  31.35 31.40    32.46 32.56 2  32.46 32.56 2  33.45 33.45 3  36.55 3  37.20 2  37.80 37.82 2  38.35 38.38 2  37.58 3	E-MAIL: b	AKETWORD	FINO-ICCOM	TELEPHONE:	
Note   Section   Note				ISEVERITY (1-3)	ADDITIONAL COMMENTS
USIZ 24.04 25.7 2 26.0 26.04 1 28.11 28.13 1 Kamir alore Road 28.11 28.13 1 30.22 30.27 3 31.35 31.44 1 31.53 31.60 1 22.46 32.56 2 33.45 33.49 3 35.21 35.22 2 36.55 3 37.20 2 37.80 37.82 2 37.58 38.38 2 37.58 38.38 3	ROUTE	A STATE OF THE PARTY OF THE PAR	The same of the sa		
30.22   30.27   3   31.35   31.44   1   31.35   31.40   1   31.53   31.40   1   32.46   32.56   2   33.45   33.45   33.45   33.45   33.45   33.45   33.45   37.80   37.82   2   37.80   37.82   2   37.58	US12	24.04	2711	+ 3	
30.22   30.27   3   31.35   31.44   1   31.35   31.40   1   31.53   31.40   1   32.46   32.56   2   33.45   33.45   33.45   33.45   33.45   33.45   33.45   37.80   37.82   2   37.80   37.82   2   37.58	/	25.4	25.	1	
30.22   30.27   3   31.35   31.44   1   31.35   31.40   1   31.53   31.40   1   32.46   32.56   2   33.45   33.45   33.45   33.45   33.45   33.45   33.45   37.80   37.82   2   37.80   37.82   2   37.58		26.0	26,04	+	Ramies above Road
32.46   32.56   2   33.45   33.49   3   35.21   35.22   2   36.55   2   37.80   37.82   2   38.35   38.38   2   39.58   3		28.11	28.13	1-1	Narrey sus
32.46   32.56   2   33.45   33.49   3   35.21   35.22   2   36.55   2   37.80   37.82   2   38.35   38.38   2   39.58   3		30 22	30,27	13	
32.46   32.56   2   33.45   33.49   3   35.21   35.22   2   36.55   2   37.80   37.82   2   38.35   38.38   2   39.58   3		31.35	31,4	11,	
32.46   32.56   2   33.45   33.49   3   35.21   35.22   2   36.55   2   37.80   37.82   2   38.35   38.38   2   39.58   3		31.53	131.60	1/	
37, 1/ 36, 55 37, 20 37, 80 37, 80 37, 58 37, 58 37, 58	+	22 46		12	DAYON SUDFHREA
37.80   37.82   2	1	133.45	33,49	13	DIG NOCA SEINCE
37.80   37.82   2	H	35.21	35.22	12	
37.80   37.82   2	1	3/ 55		3	
39,58	-	37 20		12	
37.58		3360	137.82	2	
37.58		20 75	13938	2	
NOTES:	-	29 00	78.79	13	
NOTES:		13/1.30			
NOTES:					
	NOTES:				

- 1. Ruck debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up SEVERITY:
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RICT: A	NEINO-10,COM	TELEPHONE	ON: OROFINO 208-476-4433
IL: OLAKE I COM		(	-3) ADDITIONAL COMMENTS
TE BEGIN M. P.	END ML P.	SEVERITY (	BIG ROCK + SLIDES
17/6/19	51.34	3	DIG ROCK + SEIDE
417/	41.8	12	Ja Mork
12/5/1/3	56.45	3	CORMERS
12 16 4	JAMA	12_	
10210		12	
62		1	
4110.48		12	
1198		15	
3./_	-	13	
3.49	13,5/	+3-	
371	3.76	13	BOTTOM SLIDE HAR
1 418	4,39	13	Dollow Sale
1129	6.33	12	
1.23	657	2	
2117	73	2	
3000		2	
1 37.87	1698	13	
5/2 /5.92	10/1		
1 17.95	10016	12	
19,01	19.013	9	
119.34	1/7.72		
21.9	122.00	+2	
1208	122.2	1	
1 22.55	22.63	13	
1 22.72	22.80		
1 029	1230		

1	10	T	εs	:

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EVALUATED BY: D. Stychema DATE: 8-26-59

DISTRICT: 2 ORG UNIT: ORG LOCATION: GRANGEWILLE

E-MAIL: A styce Comment, Com TELEPHONE: 1-203-798- 4281

BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
220.30	220.50	3	Some LARGE Rock
7	224.1	/	
<b>1</b>	224.5		Roling Bocks Controminate truck Range
T	SPot	1	
	Spot	,	
725.05	225.15	/	
225.6	225.7	/	
725.9	SPot	1	
226.05	226.2	/	
276.3	226.4	/	
226.5	226.65	1	
La contraction of the contractio	227.05	2	
727,2	SPot	1	
227.4	228.8	2	
228.9	SPot	2	
229.0	229.2	3	300-500 cyds of lock Fall annually
2792	229.4	2	
229.7	229.85	2	
229.95	230.1	. ,	
230.2	230.5		
230.6			
230.75	1		
231.0	231,4		W.B. Cut 1000-2000 cyds Ann
231.9	232.1	1	
	220.30 223.9 224.6 224.8 225.05 225.05 225.05 226.05 226.3 226.5 226.9 227.2 227.4 228.9 229.0 229.0 229.7 229.7 229.95 230.6 230.75 231.0	220.30 220.50  273.9 224.1  274.2 224.5  224.6 SPOT  224.8 SPOT  225.05 225.15  225.6 225.7  225.9 SPOT  226.05 226.2  226.3 226.65  226.9 227.05  227.2 SPOT  227.4 228.8  228.9 SPOT  227.4 228.8  228.9 SPOT  227.4 228.8  228.9 SPOT  229.2  229.2  229.2  229.2  229.3 230.1  230.2 230.5  230.95  231.0 231.4	220.30       220.50       3         223.9       224.1       1         224.2       224.5       1         224.6       5Pot       1         224.8       5Pot       1         225.05       225.15       1         225.6       225.7       1         225.9       5Pot       1         226.3       226.2       1         226.3       226.4       1         226.5       226.65       1         226.9       227.05       2         227.2       5Pot       1         227.4       228.8       2         228.9       5Pot       2         229.0       229.2       3         229.4       2       2         229.7       229.85       2         229.95       230.1       1         230.2       230.5       1         230.6       5Pot       3         230.95       3         231.0       231.4       3+

NOTES:

# A) Roadway protected by Port-4-Roll-Scoms to be effective

B Very Scuere and hazordous poch Fall area. Rockfall will

happen any time, Hos Been Known to close US95

Several times in the past Few Yorks.

#### SEVERITY:

001546

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EVALUAT	ED BY: D-S+	phasen	- ORGINGIENI	Cana	ATE: 8-26-58 gen-tle 1949-429/
ISTRICT:	20	RG UNIT:	OKO LOCATION	1-708-	749-4291
-MAIL:_	d orb 600	mes netico	A TELEPHONE		
	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ANDITIONA	L COMMENTS
ROUTE		Z32.7	1		
4595	232.6		1		
	233.0	233.2			
•					
		-			
		,			
	1				
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OTES:					
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EVALUATED BY: Dave Stokes DATE: 8-17-99

DISTRICT: D ORGUNIT: ORGLOCATION: Reed SA E

E-MAIL: CONSTRUCT ORGLOCATION: - 208-2795 24391

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH 14	0	6	2	
)	6	6.1	3	LARGE ROCKS
14) 新	Col	7.1.	2	
14 3	7.1	5,2	3.	Creekthat Floods And Slides Class
14/1	7. 2	17.5 %	Z	
1 2)	7.5	1716	3	Slides (Closes Road)
1	7061	7.8	2:	
	7.8	7.9	3	
4	17.9	8.5	2.	
1	8.5	8.7	3	
7	8.7	10.0	2	
<b>)</b>	10.0	10.1	3	Slide (Closes Road)
	10.1	12.8	2	
	12.8	12,9	3	Slide (Closes ROA)
1	12.9	14.7	22	
1	14.7	14.8	3	
	14.8	15.2	2'	
1	115.2	15.3	3	
4 4	45.3	16.5	2	
)	16.5	16.6	3	Slide (closes Road)
	16.6	17.1	2	/
	17.1	11.2	3	
1.	17.2	21.0	Z	
1	21.0	21.1	3	LARGE ROCKS

NOTES: Also At Mile Post 5.5 is A slide Area

#### SEVERITY:

20197

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201246-0	DATE: 8-17-99
	ORG LOCATION: REPOS 13AC
E-MAIL: distrato CAMASTEL. COM	TELEPHONE: 208-799-4281

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH14	24.3	24.4	3	LARGE RUCK
1	24.4	25.0	2	
<del>-)-</del>	25.0	25/	3	LARGE Rock
1	25./	25.8	2	
1	25.8	25.9	3	LARGE Rich
1	25.9	27.0	2	
-T	27.0	27.2	3	Slides
	27.2	28.3	2	
	28.3	28.4	3	LARGE Ruch
-/-	28.4	30.3	2	
$\overline{}$	30.3	30.6	3	LARGE ROOK
	30.6	32.0	2	· Programme and the second sec
	32.0	34.5	3	LARGERAK É Slides (closes Pa
	34.5	37.0	2	
	37.0	37.1	3	
	37.1	38.0	2	
	38.0	38./	3	Slides (closes Rds)
	38./	39.0	2	0 /
	39.0	4010	3	LARGE Rucko
	40.0	41.8	2	1
	41.8	43.0	3	LARGE Rocks & Stions
	43.0	44.0	/	
	44.0	44.1	3	
	44.1	45.0	2	
	45.0	45,1	3	

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			ICCUEDITY!!	DATE: 8-17-97  N: Reads 130  PUB 799-4291  ADDITIONAL COMMENTS	
OUTE	BEGIN M. P.	END NL P.		ADDITIONAL COMMENTS	
5414	45,1	46.3	2		
د >	46.3	42.6	3	5/1865	-
	46.6	49.8	2		_
					<b>Management</b>
					-
				·	
,					
					PROPERTY.
					-
					-
					-
TES:					
				•	

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
- 2. Rock debris occurs on the roadway several times a year with the larger rocks (> 6 inches) causing hazardous conditions during some of these events.
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	enev. D C	Laleman		DATE: <u>8-26-99</u> GRANGURILL  1-208-49-4291
VALUATE	7.	ORG UNIT:	ORG LOCATION:	Grangeelle
MAIL: d	Istop O C	EMALUEL.Com	TELEPHONE:	1-208-749-4291
			ICCVEDITY (1.3)	ADDITIONAL COMMENTS
OUTE	BEGIN M. P.	END M. P.		Applitolities collisions
SH.13	6.7	3Pot	2	
7	8.4	9.3	2	
	9.6	spot		
	9.7	spot	1	
a figh	9.8	spot	1	
	10.0	10.4	2	
	10.5	11.6	2	
OTES:		·		
				•

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EVALUATE	DBY: Jim	Pratt		DATE: 3-13-00
DISTRICT:		RG UNIT:	ORG LOCATION:	
E-MAIL:			TELEPHONE:	108 924 5602
	1	In the second	ICCVEDITY (1.3)	ADDITIONAL COMMENTS
	BEGIN M. P.	END M. P.		5'-10' ditch
The same of the sa	04,40	05-4	(1)	
5	5.6	5.8	(1)	5' ditch
5	5.8	6,3	(3)	5-10' diteh
5.	15.8	16.0	(1)	very soldom
5	20.5	21.6	(1)	5' ditch
	21.2	21.5	(1)	5' ditch
C 12	*			
11 ( 12	70.5 ~	70.65	(1)	5' ditch
45/2		71.60	(2)	(1
Annual Continues of the State o	>1.5		(2)	1,
5	72.1	72,36	(1)	1.
5	27.35	>3.15	(2)	10' ditch
3	74,4	75.0	(0.4)	10 21127
	•	7 2 2		
54 64	29.90	29.94	(1)	2 ditch
	28.10	28,4	(1)	4
3	24,50	26.9	(3)	LOW VOINING TRETS'C Slaw speck Zon Speck roak Small ditch
			·	
NOTES:				
ł				

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EVALUATED BY: Jim Pratt	DATE: 3-13-00
DISTRICT: 2 ORG UNIT:	ORG LOCATION: 025421
E-MAIL: 1+d Frais & comegnet . com	TELEPHONE: 208 924 5602

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
US 95	2795 RH	279.57 RH	1	10' ditch.
8- A	2801 LH	280.33 LH	2	5' ditch
***	280.4 RH	280.55 RH		concrete rail racks jump
<b>建一</b> 角	280.624	280 65 LH		16 11 11 11
	280.65 24	280.76 LH	2	no rail 10' ditch
	280.8 RH	280.43 RH	2	5' ditch curve
	281.07 LH	281.14 LH	2	10' ditch
	281.23 1H	281.26 LH		ip' ditch curve
	181.26 RH	281.75 RH		concrete rail rock jump
	28175 2H	281.84 11	2	5' ditch curve
	282.25 RH	282.33 AH	2	concrete rail Large rocks jump
	282.78 LH	282.85 LH	3	5 ditch
<u>.</u>	282.9 RH	283.0 RH	2	concrete rail tocks jump curve,
	284.4 RH	284.53 RH	1	concrete rail small rocks jump
	285.12 RH	285.16 RH		74 19 14 14 15
	285.82 RH	285.87 RH		5' ditch
	286.06 RH	286.1 RH	1	concrete rail small racks jump
<u> </u>	286.17 LH	286.29 LH	3	concrete sail socke jump
	286.34 LH	286.38 KH	3	11 11 11
	286.8 1H	286.88 LH	1	11 some rocks jung
	287.34 RH	287 4 RH	2	10' ditch occasional large racks
	287.7 LH	247.77 LH	J	5 ditch curve
	287.9 RH	288.06 RH	L	10' ditch curve

#### NOTES:

Except for the few number 3's we don't do a regular rock patrol unless rocks are observed + then only for a short period of time

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Sun analysisa)	DATE: 08-17-99
E-MAIL: de le Commune Contelle	OCATION: GRANGEVILLE
DISTRICT: CAMPATELE	PHONE: 799- 429/
E-MAIL: 1870	

201546

BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
184.63	184.50	/	
		2	Generally LARge Rock
		1	,
	T	/	
		1	
	19150	1	
		2	Some LARGE Rock
	The second secon	1	
		1	
-		3	Canaged 1, 1 ares Pack
	1	1	Generally Large Bock
1			Some LARGE Ruck
7	1	3	Some Large Rooms
702.70			
203.30			
204.30	204. 40		
205.20	205.40	<del>                                     </del>	0.4
205.60	705.70	2	Some large Rock
206.95	207.05		
207.80	207.90	1	
	209.60	2	Some Large Rock
	210.70	1	
	212.20	2	Some LARGE Ruck
	213.70	1	
	217.90	1	·
	The state of the s		
	184.63 188.00 189.00 189.95 190.90 191.20 192.25 193.85 196.30 197.40 198.90 201.10 202.70 203.30 204.30 205.20 205.60 206.95	184.63	184.03

NOTES:	
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	RO	OCKFALL	<b>SURVEY AND</b>	INVENTORY FORM
			2425 0 40 00	
	D BY: MARK S		DATE: 3-12-00	CA AIN IC
	ORG. UNIT 02		ORG. LOCATION FL	
E-MAIL: ma	arks@camasnet.	com	TELEPHONE: 208-92	26-4483
ROUTE	BEGIN M.P.		SEVERITY (1-3)	ADDITIONAL COMMENTS
U.S. 12	150.7	150.9	1	
U.S. 12	151.04	151.3	2	
U.S. 12	151.57	151.64	2	
U.S. 12	152.08	152.1	1	
U.S. 12	152.3	152.6	1	
U.S. 12	153.275	152.35	2	Porta-rail in one spot to catch excessive rockfall
U.S. 12	153.4	153.6	1	
U.S. 12	153.88	154.33	1	
U.S. 12	154.75	154.8	1	
U.S. 12	155.1	155.38	2	
U.S. 12	155.69	155.75	2	
U.S. 12	159.88	157.64	2	
U.S. 12	157.82	157.9	2	
U.S. 12	159.4	159.45	2	
U.S. 12	159.5	159.57	2	
U.S. 12	159.57	159.61	3	Many rocks all year long. Close to a fast corner
U.S. 12	160.57	160.73	1	
U.S. 12	161.29	161.42	3	Large rocks and on a corner.
U.S. 12	164.03	164.04	3	Large rocks and on a corner.
U.S. 12	164.04	164.2	2	
U.S. 12	164.44	164.48	1	
U.S. 12	165.22	165.36	2	
U.S. 12	165.82	165.94	2	
U.S. 12	166.38	166.56	2	
U.S. 12	166.78	167.07	2	
U.S. 12	167.07	167.65	1	
U.S. 12	168.5	168.57	3	Lots of rocks >6". On a corner causing accidents
U.S. 12	168.64	168.69	1	
U.S. 12	169.5	169.69	2	
U.S. 12	169.78	169.88	2	
U.S. 12	169.88	170.42	1	
U.S. 12	170.64	172.68	2	
U.S. 12	170.76	172.25	2	
U.S. 12	172.3	172.44	3	Many rocks on a dangerous corner.
U.S. 12	172.44	173.45	2	

	R	OCKFALL	SURVEY AND	INVENTORY FORM
EVALUATE	ED BY: MARK S	CHIETED	DATE: 3-12-00	
			ORG. LOCATION FL	EMING
DIST. 2	ORG. UNIT 02			
E-MAIL: ma	arks@camasnet.	com	TELEPHONE: 208-92	25-4483
ROUTE	BEGIN M.P.	END M.P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
U.S. 12	116.5	116.68	3	Rockslides 4-5 times a year. Rocks from 6"-48"
U.S. 12	116.95	117.34	2	
U.S. 12	117.56	117.66	2	
U.S. 12	118.12	119.26	2	
U.S. 12	119.96	120.1	3	Many accidents because rocks close to corner
U.S. 12	120.56	120.66	2	
U.S. 12	121.24	121.31	2	Large rocks on corner 1-2 times a year
U.S. 12	121.75	122.08	1 1	Large road on content is a union a year
U.S. 12	121.75	122.43	3	Several rocks > 6" in some bad corners
U.S. 12	122.43	122.43	2	OCTURE TOOKS - O IN SOURCE DAY CONTINUES
		123.83	1	
U.S. 12	123.6		1	
U.S. 12	124.18	124.24		
U.S. 12	124.35	125.45	2	
U.S. 12	124.84	125.15	2	
U.S. 12	125.36	125.58	2	
U.S. 12	128.52	121.83	2	
U.S. 12	131.12	131.24	2	
U.S. 12	131.36	131.56	2	
U.S. 12	132.16	132.65	2	
U.S. 12	132.82	133.18	2	
U.S. 12	133.66	133.87	3	Many large rocks. Many accidents
U.S. 12	134	135	2	
U.S. 12	135.6	136.135	1	
U.S. 12	136.48	136.85	2	
U.S. 12	137.1	137.15	2	
U.S. 12	137.25	137.35	3	Many rocks on the end of a corner
U.S. 12	137.53	137.6	2	
U.S. 12	138	138.28	2	
U.S. 12	139.21	139.25	2	
U.S. 12	139.81	139.9	1	
U.S. 12	139.95	139.09	1	
U.S. 12	140.58	140.75	2	
U.S. 12	141.14	141.22	2	
U.S. 12	141.77	142.1	2	
U.S. 12	142.77	142.87	2	
U.S. 12	143.25	143.47	2	
U.S. 12	144.18	144.58	1 1	
U.S. 12	145	145.2	2	
U.S. 12	145.46	145.57	1	
U.S. 12	147.73	147.83	1 1	
U.S. 12	148.065	147.83	2	
U.S. 12	148.57	148.7	2	
U.S. 12	148.89	148.97	2	
U.S. 12	149.07	148.23	2	
		148.23	2	
U.S. 12	149.7	149.9		

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Y AND	INVENTOR	Y FORM		
			0.40.00	
	DBY: MARKS		DATE: 3-12-00	
	ORG. UNIT 02		ORG. LOCATION FL	
E-MAIL: ma	arks@camasnet.	com	TELEPHONE: 208-92	26-4483
ROUTE	BEGIN M.P.	END M.P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
S. H. 13	11	11.15	1	
S. H. 13	11.27	11.555	1	
S. H. 13	11.74	12.1	1	
S. H. 13	13.85	14.2	2	
S. H. 13	14.333	14.7	3	Many and large rocks >12"
S. H. 13	16.625	17.4	2	
S. H. 13	18.3	18.68	1	
S. H. 13	19.3	19.45	3	Numerous rocks, some large, in a corner
S. H. 13	19.66	19.99	2	
S. H. 13	22.6	22.8	1	
S. H. 13	23.265	23.295	3	Numerous rocks but all small
S. H. 13	25.8	26	1	
S.H.13B	0.52	0.685	3	Many rocks, most small<6"; a few larger
S.П. ISB	0.52	0.000	<u> </u>	Have to remove 2-3 times a day in spring
				Have to remove 2-3 times a day in spring
U. S. 12	75.96	76.28	3	Many rocks on comer after every rainfall
U. S. 12	78.55	79.065	3	Many rocks small and large. Numerous accidents
U. S. 12	82.4	82.6	1	
U. S. 12	86.7	86.85	1	
U. S. 12	87	87.06	2	
U. S. 12	87.22	87.409	2	
U. S. 12	90.6	90.7	2	
U. S. 12	91.205	91.32	2	
U. S. 12	92	92.36	2	
U. S. 12	92.44	93.09	1	
U. S. 12	93.32	93.39	1	
U. S. 12	94.95	95.15	2	
U. S. 12	95.85	95.96	3	
U. S. 12	96.07	96.14	2	
U. S. 12	96.52	96.62	2	
U. S. 12	96.813	96.952	3	Numerous after rainfall
U. S. 12	96.952	97.1	1	
U. S. 12	97.666	97.676	1	
U. S. 12	99.05	99.36	2	
U. S. 12	99.94	100.07	3	2-3 Slides per year with rocks 12"-36"
U. S. 12	102.017	102.31	1	
U. S. 12	103.3	103.88	1	
U. S. 12	104.13	104.78	1	
U. S. 12	105.25	105.5	2	
U. S. 12	106.36	106.61	2	
U. S. 12	107	107.06	1	
U. S. 12	107.26	107.45	2	
U. S. 12	108.43	108.67	2	

R	out	9	beg.mil	end mil	sevenity	comments	foremen	district	location
S	HS	5	100.78	100.85	2	no to narrow ditch; limited sight	Jim Stamms	3	Valley Co.
	i					distance; decomposing material; mostly small			
						pleces; some larger pieces @ top		dan especial and a property of the	
			100.67	100.72	1	nerrow ditch; fairty solid; not too tall			
			149.9	149.95	1	no ditch; curve; large rock pieces; not tall			
			150.07	150.075	2				
						much in narrow ditch; potential for large rockfall			
			150.18	150.3	3	curve; no ditch; tall slope; high traffic; much			
						debris; different erosion rates; trees			
			150.36	150.48	3				
				energia.		curve; no ditch; tall slope; high traffic; large			
						rockfall potential; poor sight distance; trees			
-			150.51	150.595	3	narrow ditch; tall slope; high maitenance area;			
Micros	********					curve; trees			
		$\coprod$	150.6	150.65	3	патоw ditch; tall slope; high maltenance area;			<b>_</b>
	ndocara es	$\sqcup$				sandy soil; pavement damage; trees			<b>ļ</b>
			150.68	150.8	3	narrow ditch; toppling features;soil; high			
					Approximation and the second	maitenance; large rockfail potential			1
		Ш	150.88	150.93	2	narrow ditch; toppling features; some large			
		L				rockfall potential;soil			
			150.95	151	2	narrow ditch; curve; high traffic; debris on road;			
atero mare	-					some rockfail potential; soil; trees			
			151.9	151.94	3	narrow ditch; curve; large cracks; trees			
	$\perp$		151.83	151.87	3	narrow ditch; tall slope;toppling potential; trees;			-
	$\perp$					massive		<u> </u>	
	$\perp$		151.8	151.81	1			<b></b>	
-	$\perp$					no ditch; small slope; limited sight; soil; trees			
	L		151.6	151.78	2	no ditch; oversteepened slope; well graded; trees;		<b></b>	-
	Ļ					high traffic; limited sight distance		<b></b>	<b>_</b>
	丰		101.675			curve; oversteepened soil & rock		<b>}</b>	
	1		99.6	99.81	1	soil; boulders	<u> </u>		-
	1		99.48	99.53	1	soil; boulders	<del> </del>	-	-
	4	-	99.38	99.46	1_1_			+	<del> </del>
-	4	-	99.305	99.34	1_1_		<b></b>	<b>-</b>	<del>                                     </del>
_	4		99.225	99.265	1	agilt has delega		_	+
_	4		99.15	99.221	2	scil; boulders		+	<b>†</b>
_	4		99	99.05	1	curve; big rock		<del>                                     </del>	1
	+		96.8	98.975	3	soff; rack		1	
	+		97.676	98.74	2	SUR, IUUR	<b></b>	1	
	+	Transfer Printeryol	98.555	98.605	2	soil; rock	1		
-	+	-	98.4 98.335	98.515 98.37	2	soil; rock; decomposition		1	1
de const	+	nd to dispute	98.275	98.33	1	soil; rock; wide ditch	1		
-	+		95.16	98.775	-	soil; rock; oversteepened stope; decomp.		1	1
H	$\dashv$		94.89	94.955	1	curve; fimited sight; fair ditch; soil; rock	1	1	
-	$\dashv$	Projektivaj kraj	93.96	94.89	3	And the introduced artiful fam artered acred toget		1	
H	-		30.30	37.03	<del>                                     </del>	narrow ditch; curve; decomp.; cracks; tall; soil;			
H			<b>—</b>	1	<b> </b>	trees; poor sight; much debris on shoulder			
H			93.75	93.822	2	soil; decomp; narrow ditch; marginal sight			
<b>-</b>		*	93.615	93.675	3	no ditch	T	T	

17 April

Route	beg.mil	end mil	severity	comments	foreman	district	location
SHO	93.435	93.6	3	no to narrow ditch; limited sight			
\ A				distance; decomposing material; large debris;			
!				cracks			
	92.94	93.23	2	tall; narrow ditch; cracks; limited sight; large			
				pieces; trees			
	92.675	92.835	2				
				narrow ditch; cracks; overhanging in places; soil			
	92.455	92.52	2	narrow ditch; soil; large pieces; decomp.			
	92.17	92.22	2	curve; narrow ditch; tall			
	91.825	92.055	3				
				narrow ditch; curve; tall; cracks; decomposition;			
				soil; trees; overhanging rock; much debris			
	90.258	90.335	2	tall; soil; rock; porter rail; ditch; decomp.			
	89.425	89.475	1	soil; rock; wide ditch; maintenance but not really a			
				hazard			
	89.1	89.265	2	boulders; narrow ditch; soil; rock			
	88.725	88.815	1	oversteepened slope; soil; rock; tall; trees;			
				inadequate ditch; limited sight distance; curve;			
				boulders		<b>_</b>	
	80.69	80.7445	3	pavement & guardrail damage; curve;			
				decomposition; soil in joints; signs of rock friction		<del> </del>	
,				on surface			
(	90.94	80.9845	3				<u> </u>
}							

3

2	Route	beg. mil.	end mil.	severity	comments	foreman	district	location
->	SH 95	180.75	180.8	2	curve; tall slope; jointed basalt; no ditch; tress	Chartie Vipperman	3	Adams Co.
		175.1	175.2	3	tall; adequate ditch; rocks on shoulder; guardrail			
					damage; schist/granite; daylighting rock			
		174.85	174.95	2	tall slope; soil/rock; tree debris; adequate ditch;			
					erosion; debris			
		174.65	174.7	2	soil; rock; erosion rates; debris in ditch; trees			
		173.65	173.75	3	no ditch; curve; massive structures; tail slope;			
					narrow road			
		173.54	173.59	2	right side (smaller cut); decomposed material;			
					access behind outcrop; could push debris to			
2900					riverside			
get 3 -		173.53	173.61	3	larger cut (left side); randomly jointed; pavement			
2004					demage; insufficient ditch; decomposing rock;			
.77					trees; high traffic			
المه وا		173.1	173.16	2	no ditch; curve; tall slope; large debris			
		172.92	172.99	2	curve; narrow ditch; poor sight;narrow road;			
		And programmer of the Programm			overhanging decomposed material; cracks			
		143.95	144	3	north side; inadequate ditch; rotten basalt; soil			
1					interbeds; trees; curve		<u> </u>	
		143.95	144	3	north side; inadequate ditch; rotten basalt; soil			
3					interbeds; trees; curve			
		144.56	144.6	3	inadequate ditch; randomly jointed, rotten basait;			
					limited sight distance		<u> </u>	
		144.65	144.68	2	curve; poor sight; basalt; layers; soil; poor ditch;			
					brickish clay material			

	Poute Rec mil	end mil	severity	additional comments	evaluated by	date	district
	SH 21575 78.1	78.26	1	some loose rock; wide ditch	Heather	9/12/1996	3
	579 77.86	77.98	2	some loose rock; wide ditch	Grisham		
	580 81.96	82	2	one daylighting boulder, wide ditch			
	50/ 81	81.19	1	wide ditch			
	58278.34	78.44	2	gravel and cobble slide; narrow ditch			
	58378.22	78.26	1	narrow ditch			
	57,482.16	82.29	2	wide ditch			
	585 77.1	77.28	2	some loose rock; wide ditch			
	586 78.73	76.89	2	some loose rock; wide ditch			
	567 <b>75.45</b>	75.5	2	some loose rock; narrow ditch			
	58375.24	75.3	1	narrow ditch			
	599 75.07	75.15	1	wide ditch			
	590 74.75	74.8	1	narrow ditch			
	59/ 74.68	74.72	1	narrow ditch			
4	<i>592</i> 74.48	74.5	1	wide ditch			-
	593 74.29	74.46	1	wide ditch			
73)	S94 73.77	73.8	3	loose cobbles; narrow ditch			
	575 72.79	72.85	1	wide ditch			
	<i>5%</i> 70.9	71	2	some gravel slides; narrow ditch			
	591 70.75	70.81	1	narrow ditch			
	5% 70.7	70.72	1	narrow ditch			
	<i>599</i> 70.5	70.57	1	some gravel slides; narrow ditch			
9-70	600 <b>69.1</b>	69.2	1	some loose rock; narrow ditch			
U.	601 <b>82.9</b>	83	1	some loose rock; narrow ditch			
	- WOZ 18.65	18.8	$\overline{1}$	some loose rock; narrow ditch			
	3 17.9	18.1	7 2	loose rock; wide ditch; concrete rail			
172	609 92.6	92.7	1	some loose rock; wide ditch			
	us 90.8	90.9	2	some loose rock; narrow ditch			
	606 87.5	87.6	1	wide ditch			
N	607 87.1	87.2	1	daylighting rock mass; wide ditch			
(97)	608 97.05	97.2	2	,			
0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			loose sediments and rock spill ov	er ditch and g	uard rail	
	609 96.8	96.95	1	loose gravel; wide ditch			
	610 95.6	95.8	2	gravel and cobble slide; wide ditch			
	611 98.4	98.6	1	some loose rock; wide ditch			
	612 97.6	98	1	some loose rock; narrow ditch			
	6/3 97.45	97.5	2	gravel stide			
	6/4 43.55	43.63	2	loose rock; wide ditch			
	615 87.2	87.25	1	no ditch			
	W/ 43.8	43.83	1	loose rock; no ditch			
	617 86.18	86.28	1	wide ditch			
	618 100.5	100.6	2	loose rock; narrow ditch			
	<i>319</i> 103.7	103.9		loose rock; no ditch			
	620 99.95	100.1	2	loose rock; no ditch			
	621 100.3	100.4	1	loose rock; wide ditch			
	622 99.9	99.95	1	loose rock; wide ditch			
a/	623 98.4	98.6	1	loose rock; wide ditch			
`	→ 624 82.83	82.85	- 1	small gravel shote; narraw ditch			

Route	Beg. mil.	end mil.	severity	additional comments	evaluated by	date	district
 SH 52		38.05	1	both sides of road; moderate ditch	Heather	9/10/1996	3
621	38.06	38.07	1	moderate ditch	Grisham		
62	7 38.15	38.2	1	both sides of road; moderate ditch			
628	38.95	40.02	1	moderate ditch			
629	40.06	40.16	1	moderate ditch			
630	40.17	40.36	1	daylighting rock; moderate ditch			
631	40.37	40.48	1	wide ditch			
632	40.6	40.65	2	daylighting rock over soil; moderate			
				ditch			
633	41.2	41.38	1	daylighting rock; narrow ditch			

From: Keith Nottingham < KNotting@ITD.STATE.ID.US>

To: "Stan Miller (E-mail)" <smmiller@uidaho.edu>

Subject: rockfall survey

Date: Wed, 18 Oct 2000 14:35:35 -0600 X-Mailer: Internet Mail Service (5.5.2650.21)

X-Status:

Here is some data from the Maintenance Foreman in Boise:

```
SH-21 10.4 to 10.6 severity 1
SH-21 11.0 to 11.1 severity 3, jersey rail both sides of highway not enough ditch to contain-rocks are large enough to break concrete rail
SH-21 17.21 severity 2, decomposed granite, not enough ditch to contain
SH-21 17.54 to 18.2 severity 3, very large rock breaks concrete rail

SH-55 51.01 to 51.05 severity 1
SH-55 51.25 to 51.39 severity 2
SH-55 59.17 to 59.25 severity 2
SH-55 60.10 to 60.40 severity 2
SH-55 60.55 to 60.74 severity 2
```

These were from the survey form you worked out for the maintenance foreman.



EVALUATED BY:	Shan Solvenum	Howley	DATE: 8 / 3 / 99	
DISTRICT:			Mount, 10 Hailey, 10	
E-MAIL: 0/257	9 @ wall . vidoles . edu	TELEPHONE:	<del>(200) 592 101</del> 0	

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
54 75	210.5	2/0.6	鼓	scree, could be seeded to stabilize us
1	210.6	210.0	)	Pat
	210.8	211. 2	3	scree, little cotchant
	211-2	211-3	Une 1	
	211.3	211.5	82	scree
	211.5	211.6	1	
	211.6	211.8	<b>£</b> 1	tres are, little veg, steep cut, daylighting freatures. Wind curve
	211-8	2#.212.1	Z	scree, sociated away from used, some veg
	212.1	212.2	1	
	212.2	212 4	2 2	
	272.4	212. C	41	
	212.6	213.0	1	Aat
	213. 0	213.2	3	billing gave, lose debrs - almot scree, tills cake
	Z73.2	213.4	WB2	lots of veg. lay cot, lose rode > bu
	213.4	214.1	1	flet
	219-1	219.5	B 1-2	colles a bis in colohomat and road, some scree,
	214.5	8 214.9	, )	flot
	214.9	215.1	# 1	gene, no cotikent sure degree to deter
	215.1	215.8	1	
	215.8	215.9	2	
	215.9	216.0	1	
	216.0	216.3		lits of veg
	214.3	216.7	1	fiat
	216.7	216.8	2	scree, but afforts of veg. skows title occurrent afthrough debis in corelinary
1	216.8	217.4	1	flat

NOTES:
Some of the one's look bad, but they revely came alon at all.

\*\*Reform MP. 192.5 to 217° is evaluated with Zon Robinson, the maintenance freemen

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EVALUATED BY:	Shari Silveracan	Harley	DATE:	8/3/99	) )
DISTRICT:	- William Will	ORG LOCATION:	Morni, tooks	Hailey	
F-MAIL : cilugs	190 nord vidaho. edi	TELEPHONE:	(203) 892-8016		

OUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH 75	202.9	203.1	3	lose soil and small rock spilling who road, free of crosp some trees fallon and lying on roaded Au lots at veg., gaste stope, catchant
1	203.1	203.2	2	
	203. 2	203.3	1	very law cit, thrugh some loose rack
	203.3	203.4	22	1576 1867 bir and sail spolling into antibunts
	203.9	203.9	,	shallow stope, lets of very catchined, tress share signs of codes tall steep stope, vert ct, looks stable but
	203.9	204.0	1-2	tall steep stope, west cot, looks stable but some selection in catalogues, which is very guilte state, sme veg, but signs at some tall the state of cooks to the
	204.0	209-1	1-2	gentle stope, some veg, but signs at some
	209-1	209.2	<b>4</b> 3	stolete all a couple small make in control
	204.2	209.4	2	las cut slope if some longe bulders, lo
	209-4	204.6	3	scree slope willings boulder, us vegi door catchwart, attempt a case still astroys
	204. 6	204.8	2	tell, steep stoped, lots of Sil & logic rocks,
	209.8	205.0	,	
1	205-0	205.1	3	tall steep cot, seems failly stable, but be on a curve (convers)
	205-1	205.2	2	
	205.2	205.8	2-3	curve, lat of blind cames
	205.8	206.5	. 3	to W steep stope, vock dely's hills save cothwent doslighting tradition, not much
	206.5	207. 66	1	That stope
	207.6	207-6	3	scree stopes, tuge brothers, not much culture small canche burier (smaller Than builds
	207.8	208.2	1-2	
	208.2	208.5	3	tall, daylighty, factores, scree; curve > Lido curve
	209.5	208.8	1	Pot
	208.8	209.1	1681	
	209.1	209.5	1.	flat
	209.5	210.1	A 1.	scree, blind corve, no to little cotchurch
- · ·	210.1	210.5	1.5	flat

-	NOTES:	state highway 75	Mp. 210.5 to	211-8 217. 9 for n	sks
- 1	~				

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EVALUATED BY:	Shari Silverman	Aniley	DATE: 9/3/	99
DISTRICT:		ORG LOCATION:	Amor Idaho Hailes	
E-MAIL: 51/195796	& novell. urdaho. edu	TELEPHONE:	(200) 09E BOLE	

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH 75	192.9-1983	193.0	125	no ditto as continuent, river on other site of highway but road is clear - road conduction acco
SH 78	193.	193.	€1	
SH 75	194.0	194.1	2	some cutioner, love rock a 1th daylating tracks
5475	194.3	194.8	2	and roalest, loose lobers, ports wet
SH 75	195.2	195.3	2	larger racks cashy hoz. and
SH 75	195.7	195.9	2	reg graving as it no catheres
	196.3	196.4	1	large rocks, but don't fall
	196. 4	196.6	1-2 P	rocks do into realcut, some so I movement, rocks 76 miles (some hardders - losse) minor contact
	176.7	196-3	1-2	
	196. 9	197. 5	1-2	soil, little carried south (southers worm)
	197. 7	197.9	1.5-2	small cuts but low rocks > 6 in 4 soil, my gra
	198.0	198.1	M2 2	don't set cut rocks do , to cut, for soil failure 1, the cothwest
	198.1	198.3	1 6 s	In readort, I see ruch , soil , rote heard
	198.5	198.7	101	
	198.8	198.9	£ 2-3	soil, no cotobuent, telus slope, in some parts
	199.0	199.5	學3	same as above, us tolus, rock falls of the !
	199. 5	200.3	3/2242-3	Some as above but more vegetation grows a it trues near top show sign of trues
	201-0	201.1	3	slamp; in the soil, large bose horldons,
	201.1	201.6	2-3	law =, save loge Louldes
	201.6	201.7	1-2	het sprays - Suber-
	201.7	201. 3	1-2	lange rocks gentle slope, but
	201.8	201.9	2	talus, gentle slope, lots of veg
	201.9	202.1	3	steep stipe, as gatherest with @ style style land barden, uns
,	202.1	202.4	3	toll , step, roots in road
V	202.4	202.9	2-3	bots of way; tall, swenthat angled stop, some loose, once potenges a problem are small tolus slope spills and

NOTES: 0, MP. 194.1 - 5194 Says	"SLIDE ACED	NEPT 20 MILE	5" -01 -05	in creat in valve
NOTES: @ mp. 194.1 - sign says - all thin rowcords face the	Saluran River			
- see state highway 75	W.D. 210.5 to	217. 1 6 4	ake	
- see state night !		7 /14 /2		

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EVALUATED BY:	Shori Slauman	DATE:	8/3/99
DISTRICT:	ORG UNIT: Vof I	ORG LOCATION: Mose, ID	
E-MAIL: siligs	19 provell. undeho . edy	TELEPHONE: (208) 872-8010	

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
3475	159.4	159.5	2	some roots in catchest spread
	159.6	159.6	1	
	159.6	160 1985	2	
	+02	F	#	
	160.1	161-1	/	
	166. 2	161.4	1	
	161.6	161.7	1	
	161. 8	162.1	1	
	148.3	148.7		Inbolos dan but not a just
	149.5	149.6	1	No Pedelens
	152.3	152.4	(	
	152.9	153.0	1	
	153.0	153.1		
	153.9	154.1	/	
	153.6	154.7	,	
	155.7	155.	2	
	155.2	155.4	2	
	155.6	155.7	3	desh look commonly falls
				/

NOTES:				
·				
BO STATE OF THE ST				•

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
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EVALUATED BY: Shari Silverna | Hanky DATE: 8/3/99

DISTRICT: ORG UNIT: 1 ORG LOCATION: Moscow tooks Harley, 1D

E-MAIL: 210 5/10 95 79/0 moch videbiock TELEPHONE: (3+6) 872 - 8015

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH 275	217.4	217.8	2	sevel, small cotelerat, sue debis in cotelerat,
1	217-8	218.9	L	flot
7	218.9	219.1	2-3	tall, steep, some, but large catebout
	219-1	219.3	2	steep but lots of very & large cottoment,
	219.3	219.5	1	Ant
	219.5	219.9	2	some scree, some steepars, him cu. of rectful on road, large cutchmant late of flat some w/s/spe lat very stocker street, tall, no very, rocks in powers, cu
	219.9	220.6	1	flat some a/s/spe lat very whether
	220.6	221.1	3	
	221.1	221.3	2	serce, short) apas, larger cotchnect
	221.3	221.4	3	scree, tallor small catchness, sonoller banders on road run Smaller stapes, still scree
	221.4	221. 7	2	
	221.7	222.5	3	very tall, bowen, some stopes, fills ratetum
	222.5	222. 🕏 8	1	Flat (tern of Clayte)
	190.9	191.1	3	
	191.1	192.5	1	
1	192.5	197.9	2-3	
16	188.7	188.8	2	
	188.8	190,1	1	
1/	191.1	190.5	2	
	190.5	190.9	1	
1 2	188.1	188.37	2	

NOTES:		_		210.5	Δ.	,
	ક્રા	state	highway	and bo	217.4 for	notes

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				Processors and the second of the second sec

EVALUATE DISTRICT:_ E-MAIL:	D BY: <u>Yhan</u> or OR	GUNIT: Hailey	ORG LOCATION: TELEPHONE:	Henley
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH 75	130.0	134.1	1	wide cotherent, not much of a corse part is a fall rubbly through, one in cotherent > 10- 45 tall
1	131.4	131.5	) .	full has large press of subble in cataloguest, cots have
V	152.0	132.1	£ .	wide cothman, not wish of a corse perk is tell rubbly through, one in cothman > 10 - 10 t tell tell that large press of rubble in cothman, coth have wide the coth is cut back in cothman, coth have tell suff salt in back, our cut, vertically out, some rubble in rubburning cut back the rad
NOTES:				

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VALUATI	ED BY: STATE	er Silvinem,	<u>~</u>	DATE: 7 / 2/20	
EVALUATED BY: Swore Silvery DISTRICT: 4 ORG UNIT: E-MAIL:			ORG LOCATION:		
FIVIAIL			TELEPHONE:		
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS	
3475	155.8	155 .9	Ź		
	155.9	156.6	2		
	156.7	157.0	1		
	월.				
	157.2	157.4	2	delone filled ditch	
	157.9	158.1	2	delone fills ditch	
	158.2	158.4	)		
	158.85	158.97	2	debas fills ditch	
	159.0	159.4	2	<u> </u>	
	158. 7	158.9	2		
NOTES:					
				<u>.</u>	

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	n nv		1,759	DATE: 3/4/99
EVALUATE DISTRICT:		ORG UNIT: Blsu	DRG LOCATION:	
F-MAII ·	sele 25.79 month. a	old only. Diss	TELEPHONE:	(200) 072 8016
D-140400	ALL CONTRACTOR AND	/	, ILLELITIONE	
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS.
* US 30	175 8	11c.8	l l	no ries on rope contained is the protocol of Joes cal. Shot, but they been wide I
	7,100			low priority for traffic hazard
SH 75	99.9	99, \$9	2-3	loose dolors w large loose vele
377	99.9	100.6	1-2	loose of longe loose rocks, has dikh
	101.1	101.2	,	
19	101.9	101.7	3.	
99	101.9	102.9	. /	
	102.9	103.9	/	
	103.9	103.9	<b>\$</b> 2	
	103.9	104.7	1	
	104.7	39.9 105 - \$	1	
	87.9 105.3	88.1 105.5	\$ 1003 I	loss rubble, lits of fines, but large with a
	88.1	85.Z 185.6	1	
	85.2 105.6	88.4 105.B	1	
	105.9	88.5	/	
	85.6 10 <b>5</b> .9	106.1	,	•
	106.1	106.2	1	
	106.2	104.3	1	
	<del>707. 2</del>	107.3	<del></del>	
	107.4	107.5	1	
	107.5	107.8	1	
	<del> </del>			large moles

DIES:
Bliss Morapenance / Mike Ellis sord that they rouch had problems with This make bosoft readout.
The roadest stands just a few unles down the highway from the Bliss maintenance shed
-curus in most of this road

#### SEVERITY:

108.0

108.2

108.1

103.2

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SH 75 108.3 3 108.7 1 108.8 3 108.9 2/1 + 5 side 2, N side 1 - Hangle 109.3 109.7 1 111.2 111. \$3 1 111.4 111.5 1	SH 75 108.3 3 108.7 1  108.8 3 108.9 2 1  109.3 109.7 1  111.2 111.43 1  111.4 111.5 1  112.4 112.5 1  112.9 118.4 1  114.2 114.4 1  114.1 114.8 1  116.2 116.3 1  119.6 119.7 1  119.8 7 119.9 1  123.4 123.7 (  125.1 125.2 1	SH 75 108.3 3 108.  108.8 3 108.  109.3 109.  111.2 111.	7 1 9 2/1 7 1 \$3 1		
SH 75 108.3 = 108.7   1   108.8 = 108.9   2   1   109.3   109.7   1   111.2   111.4   111.5   1   112.4   112.5   1   112.9   113.5   113.6   1   114.6   114.6   114.6   114.6   114.7   119.7   1   119.87   119.9   1   119.87   119.9   1   123.4   123.7   1   123.4   123.7   1   125.2   1   125.2   1	SH 75 108.3 = 108.7   1   108.8 = 108.9   2 / 1   108.8 = 109.7   1   111.2   111.4   111.5   1   112.4   112.5   1   112.7   1   112.9   118.4   1   114.2   114.4   1   114.8   1   114.2   114.8   1   119.7   1   119.87   119.7   1   119.87   119.9   1   121.6   121.9   1   123.4   123.7   1   125.2   1	108.8° 108. 109.3 109. 111.2 111. 111.4 111.	9 2/1 1 1 \$3 1		
108.8	108.8	108.8° 108. 109.3 109. 111.2 111. 111.4 111.	9 2/1 1 1 \$3 1	s side 2, N	side 1 - Honghe
108.8°   108.7   2   7   1   109.3   109.7   1   111.2   111.43   1   111.5   1   112.4   112.5   1   112.7   1   113.5   113.6   1   114.2   114.4   1   114.6   1   114.6   1   114.6   114.8   1   119.7   1   119.87   119.9   1   121.6   121.9   1   123.4   123.7   1   125.2   1	108.8    108.7    2   1	109.3 109. · 111.2 111.	7 1 \$3 1 5 1		
111. 2   111. \$3   1   111. 4   111. 5   1   112. 4   112. 5   1   112. 6   1   112. 7   1   113. 6   1   114. 2   114. 4   1   114. 6   1   119. 8   1   119. 8   1   119. 8   1   119. 8   1   119. 8   1   121. 6   1   121. 7   1   123. 4   123. 7   1   125. 2	111.2   111. \( \frac{4}{3} \)	111.2 111.	<b>\$</b> 3 / 5 /		
1/1.4	1/1.4   1/1.5   1   1/2.4   1/2.5   1   1/2.4   1/2.7   1   1/2.9   1/8.4   1   1/3.5   1/3.6   1   1/4.6   1   1/4.6   1   1/4.8   1   1/4.2   1/4.8   1   1/9.37   1/9.9   1   1/9.37   1/9.9   1   1/9.37   1/9.9   1   1/9.37   1/9.9   1   1/9.3.4   1/23.7   1/9.5.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/25.2   1   1/9.37   1/9.9   1/9.9   1	111.4 111.	5 1		
1/2.4   1/2.5   1   1/2.6   1/2.7   1   1/2.9   1/3.4   1   1/3.5   1/3.6   1   1/4.6   1   1/4.6   1   1/4.6   1   1/4.2   1/4.8   1   1/4.2   1/4.3   1   1/9.7   1   1/9.87   1/9.9   1/9.9	112.4 112.5 1 112.6 112.7 1 113.9 118.4 1 114.2 114.4 1 114.6 114.8 1 116.2 116.3 1 119.6 119.7 1 119.87 119.9 1 121.6 123.7 ( 125.1 125.2 1	112.4 112.		1	en <sub>de</sub> species als de contratas en de l'imperiode contratas de la contrata de l'imperiode de l'
1/2.6 1/2.7 1/2.9 1/8.4 1/3.5 1/3.6 1/4.2 1/4.8	112.6 112.7 113.5 113.6 114.2 114.4 116.2 116.3 119.6 119.7 119.97 119.9 1 123.4 123.7 1 125.1 112.7 1	112.6 112			
114.6 114.8 1  116.2 116.3 1  119.6 119.7 1  119.87 119.9 1  121.6 121.9 1  123.4 123.7 (  125.1 125.2 1	114.6 114.8 1  116.2 116.3 1  119.6 119.7 1  119.87 119.9 1  121.6 121.9 1  123.4 123.7 (  125.1 125.2 1	112.9 118.	.7 /		
114.6 114.8 1  116.2 116.3 1  119.6 119.7 1  119.87 119.9 1  121.6 121.9 1  123.4 123.7 (  125.1 125.2 1	114.6 114.8 1  116.2 116.3 1  119.6 119.7 1  119.87 119.9 1  121.6 121.9 1  123.4 123.7 (  125.1 125.2 1				
114.6 114.8 1  116.2 116.3 1  119.6 119.7 1  119.87 119.9 1  121.6 121.9 1  123.4 123.7 (  125.1 125.2 1	114. b 114. b 114. b 114. c 114. c 114. d 119. c 119. 7 119. 9 1 119. 9 1 121. b 123. 4 123. 7 1 125. 1 125. 2 1	113.5 113			
114.6 114-8 1 116.2 116.3 1 119.6 119.7 1 119.87 119.9 1 121.6 121.9 1 123.4 123.7 ( 125.1 125.2 1	114.6 114-8 1 116.2 116.3 1 119.6 119.7 1 119.87 119.9 1 121.6 121.9 1 123.4 123.7 ( 125.1 125.2 1	114.2 114.			
119.6 119.7 1 119.37 119.9 1 121.6 121.9 1 123.4 123.7 (	119.6 119.7 1 119.37 119.9 1 121.6 121.9 1 123.4 123.7 (		8 1		
119. <b>3</b> 7 119. 9 1 121. L 121. 9 1 123. 4 123. 7 1 125. 1 125. 2 1	119. <b>3</b> 7 119. 9 1 121. 6 121. 9 1 123. 4 123. 7 (	116.2 116.3	/		
121. L 121.9 1 123. 4 123. 7 ( 125. 1 125. 2 1	121 · L 121 · 9 1  123 · 4 123 · 7 (  125 · 1 125 · 2 1	119.6 119.7	1		
123.4 123.7 ( 125.1 125.2 1	123.4 123.7 ( 125.1 125.2 I	119.87 119.	9 /		
125.1 125.2 1	125.1 125.2 1	121.6 121.	9 1		
		123.4 123.	7 (		
125. \$4 125. \$5 1	- 125. \$4 125. \$5 1	125.1 125.	2 1		
		125. \$6 125.	59 1		
	_				
	-				

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
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DATE: 8/5/99

EVALUATED BY: Shavi Silverman DISTRICT: ORG UNIT: Hanley ORG LOCATION: Halay DISTRICT:\_ TELEPHONE: E-MAIL:

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SH 75	51.3 75.8	75.8	1	short, really vertical, some losse rocks
1	76.2	38.0 76.5 59.7	3	serce, hall selves a newly point road, destrated to these a get top percents, burned over , land \$100 pt gall, stary, in laft get , but large to cook
	76.9	77.3	1-2	· ·
	59.8	<b>≨</b> 77.9	2-3	just autity folks to the
	78.2	78.6	23/-2	losse rate near top but mirty stable, tall, on foliaid corre daylighting true trees, see landslides
	78.7	78.9	1-2	daylighting tractives, see landslides
,	79. 3	79. 4	1	
	80.8	80.8	81	
	81.0	81-3	2	wide cotch but doppything trackers, debors on firstly junes od., corre
	81.9	82.0	1	
	82. € 2	82. 4	1-2	looks like is cont. slaughs, but it is cut back
	82.5	82.6	1	
	82.8	83.1	2	cont. sloughs into trench, cleaned recently
	g 3. z	83. 3	1-2	daylighting fractions, blocks in threach
	85.6	86.6	1	
	86.2	86.3	1-2	doglighting touchives, but is cut back it weather
	36. 7	86.9	1	vertical, cut back
	9 88.99	88.9	/	
	89.9	89.9	1	
	90.1	90.Z	1	throughout, curve , but cut back
	90 6	90.7	,	big blocks looks clean Though, veither
	71.4	91.5	/	
	91.5	91.6	/	
	91.9	92.0	1	
V	92.2	92.57	/	

NOTES: . The area rear lawaron burned in 1989

No former came at to laware with me, so severy scale is based upon sect an norty pand road, features that former in other areas possible at, and head bearings

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EVALUATED BY:	Shai Silverman			DATE:_	8/	5/9	9
DISTRICT:	ORG UNIT: Haley	ORG LOCATION: _	Hanley		7		
E-MAIL:		TELEPHONE:					

ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
SN 75	92.7 .	92.8	2	steep save dobors on other side of road, but but ditch
	93.3	93.4	l	
	93.8	94.6	1	
	94.6	94. 7	1	
	94.9.	94.9	/	
	95,6 .	95.0	1	
	95,3	95.4	1	
	95.4	\$ 95.7	,	
	95.87	95.8	1-2	tell, vertical - looks wear but
	25.9	98-0	1	
	96-0	96.8	1-2	losis like it slowly sloughs, every, correlated to soll
	96.8	96.9	2-3	
	97.0	97-1	1 ~ 3	looks really lead but has parter vail a wide trench (looks new). Chips o
	97.3	97.9		
	97.7	97.7	3	
	97. 8	97.8	3	
	97.8	98.9 97.9	2-3	
	78.0	98.0	1	
	98.1	98.2	1	
	79. 9	93.5	2-3	
	98.6	98.7	/	
	98.8	99.0	1	
	99.1	99.3	1	
	99. 4	99.6	/	
A	99.7	99.9	1	

NOTES:			
·			

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<b>EVALUATI</b>	ED BY: Som	er Divseman		DATE: 7 / 2 / 00
DISTRICT:	5	ORG UNIT:	ORG LOCATION:	Liberty to Presh they 36
E-MAIL:		chi 1971 i 1970 di tri con indicio i richi con con income con	TELEPHONE:	
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
51+ 36	24.5	24.5	21	good dit h I some weekenging with
1	23.4	23.5	1	Good All Charles Daniel La son
	23.0	23.2	1	Ausme
	22.3	22.4	1	aloud ditak
	21.0	21.1	1	<b>1</b>
	20.9	20.9	i Na	1 little landflow fil sitch frage
	19.8	19.9	1	1.44
	19. 4	19.5	ı	tot very cooled / lop of debns in loss
<b>V</b>	19.0	19.1	1	to very ended /lop of debns in look
MOTEC			PP (1 м. 1 м	•
NOTES:				
				1

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OUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
US 89	30.41	30.3	1	no place to stop
	30. 5	30.7	2	
	30. 9	3/-0	Z	V
	21.0	<del>35.23</del> /./	2	Noylighting Ins ruces
	31. 2	31.3	2	no place & sho
	31.4	31.5	2	
	32.0	32.1	2	
	32.2	32.3	1	\$
	32.6	32.7	2	no wholf debris in ditch
	32.7 .2	32.8	2	
	33.2 .0	33.3	2	1
	33.3	33.4	2	Their 15 A PULLOUT / deposes who
	34.0	34.1	2	no pullant / delans in John
•	34.1	34.2	2	/ /1
	34.3	34.6	2	
	34.6	34.87	2	V
	39,7	34.9	2	There is a gillout / Sebris in date
	34.9	35, A	2	no gollon't forbors in ditch
	35.8	35 , 9	3	no willant / debos in ditah /tall
	34.2	36.4	2	
	36.4	36.6	2	
	37,0	37,1	3	daylighting files Slabs / no pollout / deb. in a
	37.	37, 2	A 3	s. s.de of cit = 3
	39,8	3908	1	no ostlant /close to fenero / depor atoh

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EVALUATE DISTRICT:_ E-MAIL:	DBY: Angela 5 JOR	Taylor GUNJT:	ORG LOCATION:		
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS	,
I-15	56,557	55.83	1	basalt w/ = Fd. mentary over	lam
I.15	26	26.	1	/ 0	
SH-36	118.5	19			
SH-36	114.2	114,8	1		
SH-36	13.6		1	Left Sido	
SH-36		20,921			
()C-91	29.5		1		
SH-360		5.6	ĺ	right Side	,
SH -34	25.5	26	2	7.7.0	
SH-34	107	26 108			
SH-36	12.5		)		
34-36	13.8	14	,		
54-36		15.8	/		
54-36	The second secon	, , , ,	1		
H-36	16,5	17	,		
SH-36	175	_	1		
SH-36	17 10	17.7	1		
54-36	23,4	23.8	1-2	applications hedding + inin	to
54-30	4451	2000	2	daylighting bedding + pin	~
15-89	26.3	40	2-3	under construction	
US-30	375.1	375.2	1	old the spad ~ 10-15'	
US-30	371.2	371.5	1-2	Harried use barrier	
15-30	361.9	362	1	0	
T-15	528	52.9	,	S.BOUNDIANE, CUT N4-	51 H
SH-34	105	106	/	Sita ones (Ande, Cor	
1211 21	10)	1110			
NOTES:			ne a mano a copporte mineral del riches por je propos discoppo prima ameritario a differenti del 1977.		
				•	

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EVALUATE	D BY:	el Silvelman		DATE: 7 3 00
		ORG UNIT:	G LOCATION	: on SH 34 BETWEEN PROSTON & TO
E-MAIL:			TELEPHONE:	215 5 of laken N dand St 36:
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
5# 34	25, 1	25.2	1	some vetele some shalles &
	25.8	25.9	1	same satisfact ".
	25.9	26.0	2	cont tookshote / corre / narrow &
				, ,
SH 91	29. 4	29.5	1	Right side -
	29.5	29.6	l	Right side
	29.6	29.7	1	kft sik
I-15	55.1	55.3	ı	N bomi good shouldor
	56.0	56.3	1	14 /-
SH 86	114.1	114-2	1	
	114.2	114.3	1	
	114.6	114.817	2	hope bulies / some small blocks on vo
· Entertaine de l'Anna				
NOTES:				
NU 1 E3:				

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-MAIL:	ED BY: Ange		TELEPHONE:	
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
	-	1 6-15		
SH-37	50		/	
I-810	57.5		1	·
75-89	30	37,6	1.3	
H-310	19	23.6	3	
Charles and Section 1864				
		·		
NOTES:				

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EVALUATED BY: A. Taylor  DISTRICT: 5 ORGUNIT: ORG LOCATION:  E-MAIL: TELEPHONE:									
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS					
I-15	57	55	1						
I-15	26	24	,						
SH-36	112.5	114	/						
SH-36	114.2	114.8	,						
SH -36	Control of the last of the las		1	left Sido					
5H-36	20.8	20.7	1	0.					
54-91	29.5		/						
SH-36	5.5	5.6	1	right side					
5H-34	25,5	26	2						
54-34	107	108	/						
			·						
				-					
NOTES:									

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### IDAHO TRANSPORTATION DEPARTMENT - DIVISION OF HIGHWAYS <u>ROCKFALL SURVEY & INVENTORY FORM</u>

		EVALUATE	ED BY: <u>JON L</u>	D. KISHITAMIA	****	DATE:
		DISTRICT:		RG UNIT:	ORG LOCATION:	
	<i>C.</i>	E-MAIL:		The account of the contract of the present of the account of the contract of	TELEPHONE:	
	Score	ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
	211	SH-31	12.893	13.176	1-2	sight distance 216 around curve
\		SH-31	13.293	13.556	1-2	Sight dist. 183 on curve, Clean 1x
)		3H-31	11.769	11.808	1-2	1 794 chara curio 42 1
older		SH - 31	14.446	14.597	1-2	207 sight on curve, 5% grade
/		SH-31	15,766	15.967	1-2	483 Cinul 3% grade clean 15-
. /		SH-31	9.326	9.374	1	717 Sight, long curve - Sight a clean 1x ur-
		SH-31	10.369	10.437	1	Sight as, clean 1x ur.
		SH-31	7.259	7.329	1	sight 780' in clurve clean /xur
	[489	115-26	388.850	389.398	3	sight 345' no catchment in areas
*	,	The second secon	374.255	374.797	2	Sign+ 363' 1-2xur cleanup
			374.070	374.213	2	Sant 195' Sharer urve
Juce .	1 1		391.427	391.684	1-2	Fight 339 5% grade 1xHr clean
chron	237	US-26	386.869	387.140	1-2	59ht 1590', 5% a rade clean 14/4-
1	237	US-26	397.801	397.920	2	sight 816 5% arado clean Min
	213	US-26	390,690	391.214	1-2	11/475' 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		US-26	388.023	388.465	• 1	325 Curve, 5% grade ck daine cle.
1.	1	US-26	387.310	387.868	1	118 Stognade Mean Hun
	141	05-26	368,700	369,179	1-2	789", 6% gade, CIVIE
Z.081	4					,
ly Bogai	ררוא	US-93	19,905	140.670	/	424' Sight, Wirding rd
h		51+ 47	11.411	11.610	2+3	Clan 2x/yr, ck 2x/day, sight 150,
W Jek		dilliani de la constanta de la	11.941	12.319	2-3	170'sight, Cirve Clean 2 Hyrck 2x/day
Chin.	263	US 20	345.431	365.699	2	1720'sight (r% grade 2x/yr 2x/day
	ſ	NOTES:				
		NOTES:			÷	
					•	
			•		•	
	1					

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		EVALUATE	DBY: JON D.	KISHIYAMA	1	DATE: 6/23/98	
		DISTRICT:_	OF	RG UNIT:	ORG LOCATION:		
		E-MAIL:			TELEPHONE:		
	Scorp	ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS	l
			366.595	366.852	2	Sight 570 long curve, 6% grade	2×/m 2×/day
, ,h	1		366.876	367.311	2	375' Innacione 6% grade 2*hur	Palla
Herb	221	115-20	367,544	368.246	2	375', lorgewere 6% grade 24/yr, 531' lor of curve lomanake Zun,	2×/day
Diexle	203		364.135	364,428	2	960, 6% grade, 2×/m. 2×/dan	100
. !		SH-32	7.979	8.068	1-2	1200, 6% grade, 2×/yr, 2×/day	A =
						, ,	
Challis	(411	US-93	266,376	267,268		243, windingsect, Mult. Clean u	din
Section	¥393	US-93	273.445	273.649	3	204 Sharo airue 2x/4r. ha	Eards 3-4
0.11	<b>VS87</b>	US-93	148,733	150.090	1-2	292' Winding 5% grade, Stable	14, 1x/m
Vermas	357	US-93	264,467	264.713	2-3	2731, winding severalx/yr	
Ne.	900		222.869	223,373	2	330 wirding 1-2×/ur	
		THE RESERVE THE PARTY OF THE PA	271,919	272.257	2	159, Sharocitie 2x/m	
			220.652	227.539	2	618' wirding, 1-2x/yr	
	301	US-93	259.588	260.051	2	301 longhazard area wirdin	a
,	1301	SH-75	731.452	231.754	2-3	456, Chirul, 2x/yr, hazard	0
<b>J</b>	¥ 2,83		218.880	219.112	1-2	546 Curve 1-2xlur harrier	retains :
			236,269	236.501	2	174", whiding balday of the	14 across
,			263,870	269.141	3	777	1 /// 66
			270.684	270.816	2	760, curve, 2×/yr, reg. achi	1/2
	·	The same of the sa	267,534	267.687	2-3	237 winding Sev. Xip reg a	chinter
	4/200	5H-75	223.487	224.275	2		
,			239,832	240	2	726 Inna circle Ixlyn 720 wirding 2×14, reg. ac 303 curve 2×14	
	,	The state of the s	269.751	269.912	2	1720 wirding 2x/yn, reg. ac	tinity
			225,667	225.859	2		1
	223	<u> 105 - 93</u>	258,879	259.177	2	1426, winding, 1x/in reg. actin't	ky
		NOTES.				0 ,,,	1
		NOTES:					
						•	
			•	•			Py underproduction .

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	EVALUATE	DBY: JON D.	KISHIYAMA		DATE: 7/9/98
	DISTRICT:_	OR	G UNIT:	ORG LOCATION:	
	E-MAIL:			TELEPHONE:	
	ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
1223	15-93	260.821	261.361	1-2	384 wirding /x/yn
1211	SHIS	232.840	232,964	1-7	941, long curve 1x/m
	SH-75	224.566	224.810	1	1200; long curie 1-2 x/m regardinity
11,05	1.00	257.757	257,838	1-2	525 curve, 1×/m
1 as 211 em 205	SH-75	236,664	236.785	1	510 longcurve 1-2x/m
W.	15-93	258.081	258.288	1	1014, 1x1m
187 133	US-93	2103.494	263.701	1-2	3391 winding, 1×/42
731	SH-75	219.838	219.924	1-2	411" curve, F2x/y, potential for & rx
127	SH-75	235.021	235.229	1	Sight ~ 00 1-2×/yr
121	5H-75		725,220	1	606, curve 1-2×/m
:  Vermas41	15-93	297.402	298,359	3	585 winding section (INVE 38/ Juriclean accide
mIMON 37		286,452	284,486	3	1280 winding shorocurve lots of activity
Section 357		293.186	293.667	1-2	1717 / WIROLING PORO CLIPVE CX/UN CLEAN-US
*337		281.487	281.887	2-3	1509 winding shows curry 100 activity sev. Xhim
315	1 1	296.552	296.717	1-2	387 sharp: Curve "no catchment fall in road
* 303		319.434	319.727	3	1000 000 100 00 100 00 00 00 00 00 00 00
* * 303	XX	324.267	324,750	K 3+	849 winding SEV XI un clean the of a fish of the series of
303		287.457	287.894	2	
303		289.985	290.810	2-3	336' 3x/y a lot of a chistry
<b>₩</b> 303		283.109	283,499	2	291', sharp curve, several x/y
303		294.250	294.038	2	348 2x/m winding reg. activity
285		24.479	314.990	1-2	546' winding 2x/up a Pot of activity
275		316.757	317,403	2	570, winding sev. XI'm rea activity
285	115-93	318,440	318.836	1-2	1828; Wirding, long curve, sev. X y, parrier
	_				Catchie
	NOTES:				

\* Forman concerned areas' \*\* Raters next choice to be fixed

- 1. Rock debris occasionally sloughs onto the roadway, with a low volume that usually requires only minor clean up
- 2. Rock debris occurs on the roadway several times a year with the larger rocks (> 6 inches) causing hazardous conditions during some of these events.
- 3. Rock debris occurs on the roadway frequently or in such a manner that would create a hazardous condition, such as rockfall on a curve. Such locations often require immediate attention during or after storm activity.

DATE.

TABLE VICHIYAMA

	Γ:0	KG 01411	TELEPHONE:	
-WIAIL:			I ELEFTIONE:	
ROUTE	BEGIN M. P.	END M. P.	SEVERITY (1-3)	ADDITIONAL COMMENTS
B93	3 295.935	296.220	1-2	606' 2x/y, winding, reg active 612' long curve, 2x/yr
1	297.084	277.810	1-2	Col2 long curve 2x/m
	280,308	280.374		489' winding Sharp curve, 2x/yr
	284.805	285.347	1-2	1270' Winding Sharo curve Seux
	321.368	322.145	2	(200', wind, no, 2×/4, auts aces le
	274.741	275,209	1-2	12410' long curve 2x/ yr
	340.024	340,860	0-1	17/7 5% grade wirding Zx/yn u
	325.308	325,308	1-2	7/7/5% grade wirding, Zx/y, 2 258, winding, 2x/y
	279.427	279.598	1-2	711 winding 2x/m
	341.728	341.473	0-1	578, winding 5% grade, Extynu
	344.763	344.914	0-1	597' winding 7x/in FHAdigu
	338.600	339,160	/	13 / Wiraina Made, /x/yn,
	347.687	347,604	0-1	588, wirding 5% grade 2x/4p.F.
	292.100		1.	351', winding 2x/yr dayighting 5 12 winding Sharp Clima 2x/y
V	282.055		1-2	342 winding sharpling 2x/
15-7	3324,019	326,133	1-2	(dd) winding /x/yr
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MICHEL PROGRAMMENT MANAGEMENT AND ADMINISTRATION OF THE PROGRAMMENT AN				
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	CONSTRUCTOR OF THE PROPERTY OF			
OTES:				

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# Appendix B Rockfall Hazard Rating Form

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RC	A	D_			_	FROM M. P		TO M. P		
EVALUATED BY							DATE			
RC	ROADCUT HEIGHT ROADCUT WIDTH									
RATING POINTS 1 POINTS 3					POINTS 3	POINTS 9	POINTS 27	POINTS 81	SCORE	
		Traffic (ADT)		< 200	200 - 500	500 - 1000	1000 - 3000	> 3000 Very Limited		
Sight Distance			ght Distance	Adequate Stopping Distance Full Shoulder	Good Visibility & Shoulder Width	Moderate Visibility & Shoulder Width	Limited Visibility & Shoulder Width	Visibility & Shoulder Width		
Maitenance/ Clean Up			nance/ Clean Up	< 1 day on site disposal	1 - 2 days on-site disposal or < 1 day off-site disposal	3 - 4 days on-site disposal or 1-2 days off-site disposal	> 4 days on-site diposal or 3 -4 days off-site disposal 25"-35"	> 4 days off- site disposal		
I	re	cip	itation/ Climate	< 10" Precipitation Mild Winters	10"-15" Precipitation Some Freeze/ Thaw	15"-25" Precipitation Short Freezing Periods	Precipitation Long Freezing Periods	>35" Multiple Freeze/ Thaw		
	D	itc	h Dimensions	Meets Ritchie's Criteria	Adequate Width Inadequate Depth	Moderate Catchment (50- 90% Width)	, , , , , ,			
1		•	y Width Including Shoulders (feet)	> 44	38-44	30-38	30-38 22-30			
G E	н		Structural Condition	Massive, No Fractures Dipping Out of Slope	Discontinuous Fractures, Random Orientation	Fractures from Wedges	Discontinuous Fractures Dipping Out of Slope	Continuous Fractures Dipping Out of Slope		
0 L 0	A Z		Rock Friction	Rough Irregular	Undulating	Planar	Smooth Slickenslides	Clay Gouge Faulted		
G I C	A R D	Α	Structural Condition	None or 1 Differential Erosion Features	Few Differential Erosion Features	Occasional Erosion Features	Many Erosion Features	Major Erosion Features		
A L	S	S E 2	Difference in Erosion Rates	No Difference or Very Small Difference	Small Difference	Moderate Difference	Large Difference Favorable Structure	Large Difference Unfavorable Structure		
	:	Slo	pe Continuity	No Launching Features	Possible Launch Features	Some Minor Features	Many Launching Features	Major Launching Features		
	enone e	]	Block Size	<6 inches	6-12 inches	1-2 feet	2-5 feet	>5 feet		
PARTICULAR PROPERTY OF THE PRO	R	ock	sfall Frequency	< 1/ year	1 - 3/ year	4 - 10/ year	Often & After Significant Storms	Very Often (< weekly)		
NAME OF THE OWNER, OF THE OWNER, OF THE OWNER, OF THE OWNER, OWNER, OWNER, OWNER, OWNER, OWNER, OWNER, OWNER,			Priority				Total S	core		
(	Geological Characteristics:  Case 1: - Joints, bedding planes or other discontinuity is the dominant structural feature.  Case 2: - Differential erosion is the dominant structural feature.									
Remarks/ Photo Listings:										
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